

## Supporting Information

### Nanostructured Copper Interfaces for Enhanced Boiling

Chen Li\*, Zuankai Wang\*, Pei-I Wang, Yoav Peles, Nikhil Koratkar\* and G. P. Peterson\*

[\*] Prof. N. Koratkar. Corresponding-Author, Z. Wang, Prof.Y. Peles,  
Department Mechanical, Aerospace and Nuclear Engineering  
Rensselaer Polytechnic Institute, Troy, NY 12180, USA  
E-mail: ((koratn@rpi.edu))

[\*] Prof.G. P. Peterson. Corresponding-Author, Dr. C. Li  
Department of Mechanical Engineering  
University of Colorado, Boulder, Co 80309, USA  
E-mail: ((Bud.Peterson@Colorado.EDU))

Dr. P.-I. Wang  
Department Physics, Applied Physics & Astronomy  
Rensselaer Polytechnic Institute, Troy, NY 12180, USA

(( \* These authors contributed equally to this work ))

### Calculation of Heat Flux and Wall Superheat

The data from the pool boiling experiments were categorized to obtain two main parameters; the heat flux ( $q''$ ) and the wall superheat ( $T_w - T_{sat}$ ). The heat flux dissipated through evaporation/boiling under steady state conditions was obtained as follows:

$$q'' = \frac{K_{cu} [(T_{TC3} - T_{TC2}) + (T_{TC2} - T_{TC1})]}{2t_{hole}} \quad (1)$$

Here the terms  $T_{TC1}$ ,  $T_{TC2}$  and  $T_{TC3}$  represent the temperature for the three K-type thermocouples ( $TC_1$ ,  $TC_2$  and  $TC_3$ ) that were used to monitor the axial temperature distribution

in the copper heater. The separation between the sensors was  $\sim 10$  mm ( $t_{hole}$ ) and  $K_{cu}$  is the known thermal conductivity of Cu.

The wall temperature ( $T_w$ ) and the liquid saturation temperature ( $T_{sat}$ ) were expressed as follows:

$$T_w = T_{TC1} - q'' t_{STC1} / K_{cu} \quad (2)$$

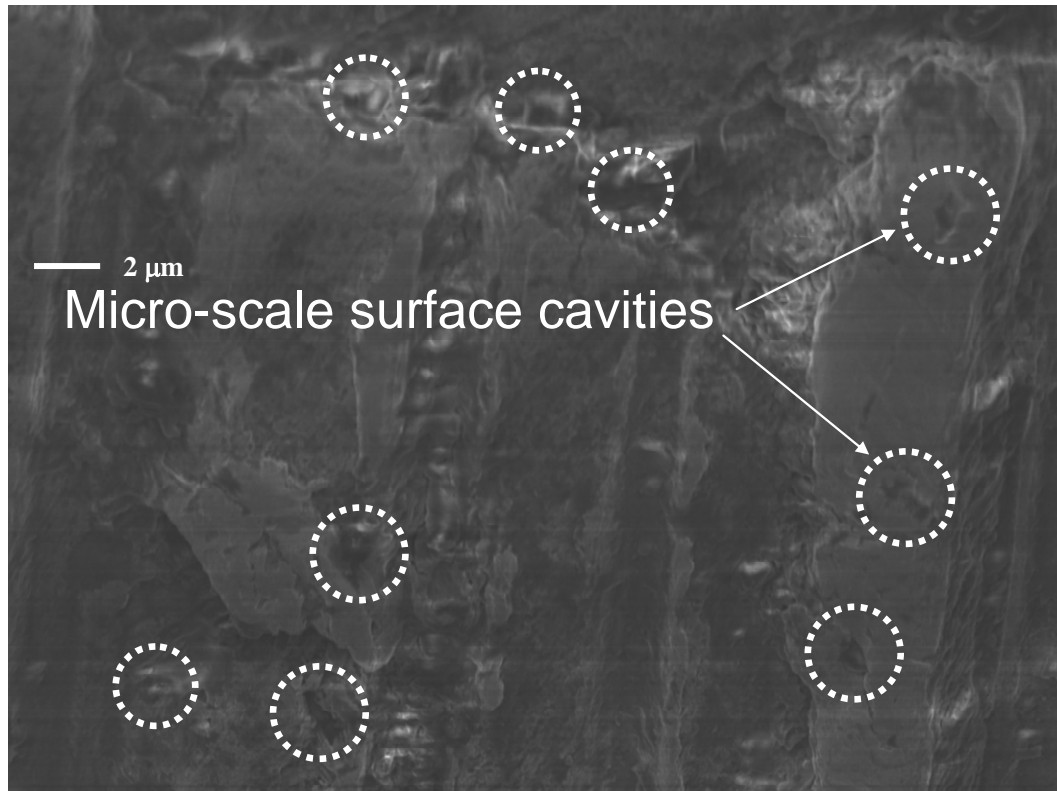
$$T_{sat} = (T_{TC4} + T_{TC5} + T_{TC6}) / 3 \quad (3)$$

where  $t_{STC1}$  was the distance between the TC<sub>1</sub> sensor and the solid surface ( $\sim 0.5$  mm). The terms  $T_{TC4}$ ,  $T_{TC5}$  and  $T_{TC6}$  represent the temperature for the three thermocouples (TC<sub>4</sub>, TC<sub>5</sub> and TC<sub>6</sub>) that were used to monitor the water temperature in the test chamber. The wall superheat was then estimated using the relation:

$$T_w - T_{sat} = T_{TC1} - (T_{TC4} + T_{TC5} + T_{TC6}) / 3 - q'' t_{STC1} / K_{cu} \quad (4)$$

### **Naturally occurring microscale cavities on Cu surface without nanorod deposition**

In spite of mechanical polishing, the copper (Cu) substrates on which the Cu nanorod depositions were performed were not perfectly smooth and were populated with microscale surface features and cavities as indicated in the scanning electron microscopy image shown below. Without the stability provided by the nano-pores, these naturally occurring microscale cavities were unable to support stable bubble nucleation at low superheated temperatures (Fig. 2b in Manuscript). We expect this is because the micro surface defects are unable to effectively trap air to form gas-liquid interface and are readily flooded upon introducing water or after a short operation at high heat fluxes.



**Figure S1.** Scanning electron micrograph of the plain Cu surface prior to performing the nanorod depositions.